



ELSEVIER

00 April 2002

Optics Communications xxx (2002) xxx–xxx

OPTICS
COMMUNICATIONS

www.elsevier.com/locate/optcom

Theoretical investigation of active fiber Bragg grating

G.G. Karapetyan^{a,*}, A.V. Daryan^b, D.M. Meghavorian^b, N.E. Gevorgyan^a^a Cosmic Ray Division, Yerevan Physics Institute, Yerevan 375036, Armenia^b Fiber-Optics Communication Group, EPYGI Lab AM, Yerevan 375026, Armenia

6 Abstract

Active uniform fiber Bragg grating (FBG) written in the Er-doped or Er:Yt-co-doped fiber is theoretically investigated. We found that when pumped, two symmetric maximums arise in the reflectivity spectrum of such an FBG near the edges of its bandwidth. By increasing the pumping rate these peaks grow, and at a critical pumping value they diverge, which indicates lasing onset at wavelengths that correspond to the peaks. By further increasing pumping, lasing ceases at the first wavelengths and begins at another pair of wavelengths. Thus, lasing wavelengths change through a set of discrete values depending on the pumping rate. At the same time, conventional negative phase slope of reflective function becomes positive in the regions around the lasing wavelength. Proposed active FBG can serve as a narrowband filter or multi-wavelength switchable laser in DWDM technique. Positive phase slope in such active FBG can be used in novel approaches to increase the performance of interferometric sensors. © 2002 Published by Elsevier Science B.V.

16 *Keywords:* Fiber lasers; Bragg gratings; DWDM technique; Phase slope

17 1. Introduction

18 Doping of an optical fiber core with rare-earth
19 ions gives both a low propagation loss and inter-
20 esting laser properties. Many configurations of fiber
21 lasers using FBG were proposed and investigated
22 [1]. The ability to incorporate gratings within the
23 doped fiber with low loss, wavelength selectivity,
24 and insensitivity to outside perturbations has revo-
25 lutionized fiber laser technology. Distributed
26 feedback (DFB) lasers using UV-written FBG on
27 doped fibers feature highly stable frequency and
28 high power operation, thus they are promising for
29 applications in optical fiber communications as well

as fiber sensor systems [2,3]. Different modifications 30
of these lasers have been investigated, based on the 31
conventional lasing scheme of an active medium 32
between two FBG, serving as the mirrors. In this 33
paper, we investigate a new variant of fiber laser, 34
which is based on uniform FBG written in the rare- 35
earth-doped fiber, and show that under certain 36
values of pump rate the FBG becomes a laser, 37
emitting at wavelengths from a set of discrete 38
wavelengths. The calculations are carried out by 39
coupled mode equations (CME) method [4], which 40
is the conventional tool for FBG investigations. 41

2. Principal expressions 42

According to CME method, the electric field E 43
of the light in FBG is expressed as the sum of two 44

* Corresponding author. Fax: +3741-344377.

E-mail addresses: gkarap@crdlx5.yerphi.am (G.G. Karapetyan), ara.daryan@epygilab.am (A.V. Daryan).

45 counter-propagating waves (modes) with slowly
46 varying amplitudes as follows:

$$E = u(z) \exp(ikz) + v(z) \exp(-ikz). \quad (1)$$

48 Here $k = \omega n_{\text{eff}}/c$, $n_{\text{eff}} = n + i\alpha$, c is the speed of
49 light in vacuum, α is a coefficient describing either
50 absorption if $\alpha > 0$, or gain when $\alpha < 0$ under the
51 influence of external pump. Refractive index n
52 changes within the FBG (in region $0 < z < L$) as

$$n = n_0 \left(1 + \frac{\Delta n}{2} \cos(2\pi z/\Lambda_B) \right). \quad (2)$$

54 Here Δn is the depth of refractive index modulation,
55 Λ_B is Bragg wavelength.

56 Functions $u(z)$ and $v(z)$ describe amplitudes of
57 counter-propagating modes, satisfying the follow-
58 ing CME:

$$\begin{aligned} \frac{du}{dz} &= i\mu q v \exp(-2iKz), \\ \frac{dv}{dz} &= -i\mu q u \exp(2iKz), \end{aligned} \quad (3)$$

60 where $q = \omega(n_0 + i\alpha)/c$, $K = q - \pi/\Lambda_B$, $\mu = \Delta n/4$.

61 In the case of a nonuniform FBG, where μ or
62 Λ_B are not constant quantities but depend on z ,
63 these equations have no exact analytical solution.
64 However, several useful asymptotic approaches
65 (WKB approximation [5] and the more advanced
66 R approximation [6]) and numerical methods for
67 their evaluation have been developed. In our case
68 of a uniform FBG the depth of refractive index
69 modulation Δn and its period Λ_B are assumed to
70 be constant quantities, i.e., we consider the FBG
71 without chirp and apodization. In this case, the
72 solution of CME (3) is obtained exactly analytically,
73 that result to the following expression for
74 reflective function r of FBG:

$$\begin{aligned} r &\equiv \text{Re}^{i\varphi} = \frac{v(0)}{u(0)} \\ &= -\frac{\mu q (1 - \exp(2iQL))}{Q + K + (Q - K) \exp(2iQL)}, \end{aligned} \quad (4)$$

76 where $Q = (K^2 - \mu^2 q^2)^{1/2}$, $R = |r|$, $\varphi = \arg(r)$.

77 3. Calculation results and discussions

78 Reflective function of FBG has been investi-
79 gated by numerical evaluation of (4). For several

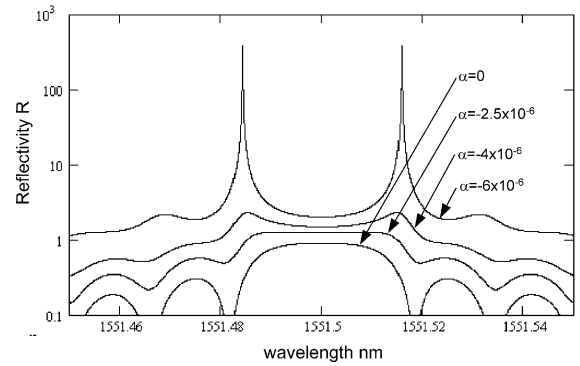


Fig. 1. Evolution of reflectivity spectrum. $L = 2$ cm, $\mu = 0.00005$.

values of gain coefficient α reflectivity R spectrum 80
was calculated (Fig. 1). As it is seen, when α be- 81
comes negative (it means that a pump is applied) 82
two symmetrical maximums near the edges of 83
FBG reflection band arise. These maximums grow 84
when pumping increases. In this case, the active 85
grating becomes a narrowband filter, or amplifier. 86
This phenomenon was described earlier in [7] and 87
proposed for the implementation in the OCDMA 88
coder and decoder [8]. The locations of the maxi- 89
mums are coincident with the grating transparency 90
points with small shift toward the central wave- 91
length. The dependence of maximum reflectivity 92
on the gain coefficient is shown in Fig. 2. When α 93
reaches some threshold, the reflectivity diverges, 94
which indicates the onset of lasing in two sym- 95
metrical wavelengths. Further increase of the 96
pump rate ceases lasing, causing it to resume at 97
another pair of wavelengths. Three-dimensional 98
image in Fig. 3 clearly shows this behavior of re- 99
flectivity spectrum proving that an active FBG has 100
a discrete spectrum of lasing wavelengths. Hence, 101
by choosing an appropriate value of pump rate, 102
one can obtain a desirable lasing wavelength 103
within a set of discrete values. This is the main 104
distinguishing feature of the proposed laser in 105
comparison with earlier investigated DFB lasers. 106
Such kind of behavior of lasing wavelengths upon 107
pumping rate can be explained qualitatively as 108
follows. The lasing is possible when the gain is 109
above the minimum value necessary in power 110
consideration, and when the phase advance of the 111
waves along FBG is equal to integer number of π . 112

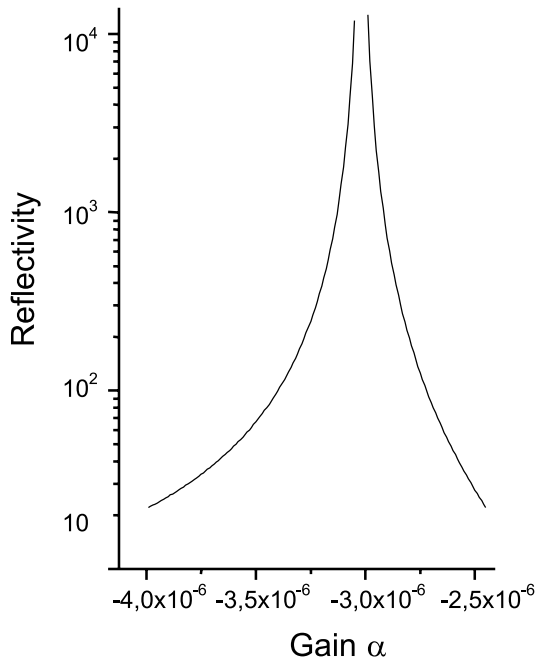


Fig. 2. Maximum reflectivity versus gain α . $L = 3$ cm, $\mu = 0.000025$.

113 These two conditions can be satisfied together in
114 discrete values of wavelength. Suppose that by
115 increasing of the gain the first lasing wavelength is

reached. Further increase of gain changes the
phase advance, because phase velocity of coupled
modes depends on both real and imaginary parts
of refractive index. As a result, phase condition is
violated and therefore the lasing ceases. Next las-
ing arises at the gain value when the phase advance
in some other point converges again to integer π .

Figs. 1 and 3 show that the increase of pump
rate results in inversion of the reflectivity spec-
trum, i.e., the minimums become maximums and
vice versa. The approximate values of lasing
wavelengths are found from (4), where transpar-
ency points are determined by the condition Re
 $(QL) = \pi m, m = 1, 2 \dots$

$$A_m \approx 2n_0 A_B \left(\frac{1 - \mu}{1 \pm \sqrt{\mu^2 + (mA_B/L)^2}} \right). \quad (5)$$

Actually, the lasing wavelengths are slightly shif-
ted from transparency points in direction of the
central wavelength. The value of α that provides
lasing depends on the FBG length and modulation
depth. The stronger the FBG, the lower the gain
required for lasing (Fig. 4). For convenience, the
values of α can be expressed using the intensity
amplification A of 1 m of that fiber from which the
FBG was made, by using the formula:

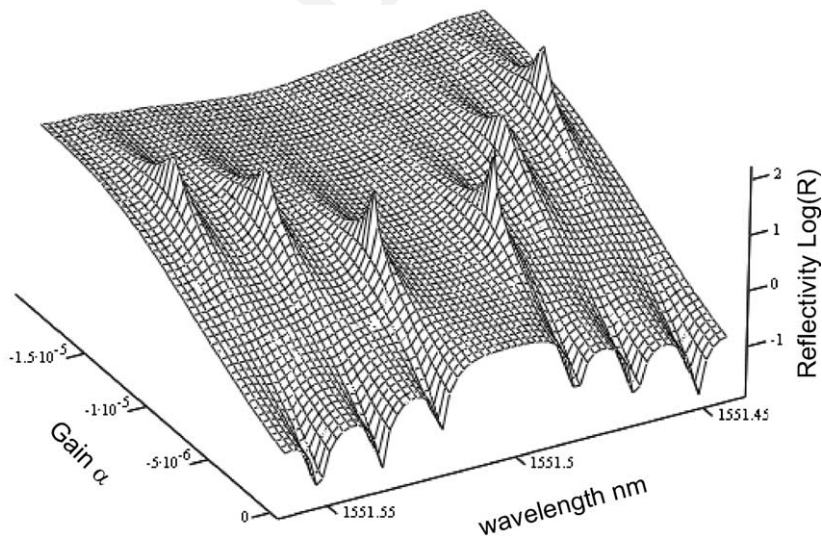


Fig. 3. Reflectivity evolution versus gain and wavelength. $L = 5$ cm, $\mu = 0.000005$.

4

G.G. Karapetyan et al. / Optics Communications xxx (2002) xxx-xxx

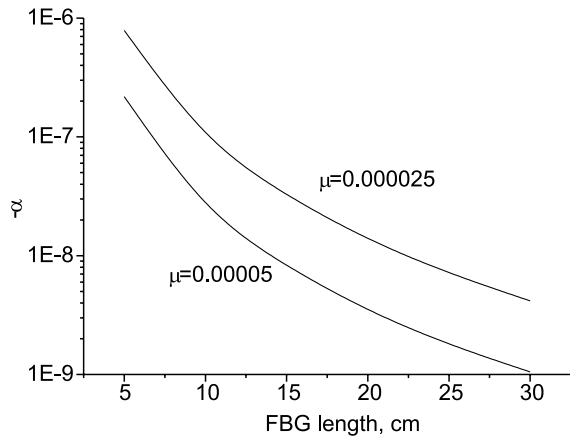


Fig. 4. The values of gain providing lasing versus FBG length.

$$A \text{ (dB/m)} = 20 \lg(\exp(-2\pi\alpha/L)) \approx -3.5 \times 10^7 \alpha. \quad (6)$$

141 Then, for example in an FBG with length 5 cm and
142 refractive index modulation depth $\Delta n = 0.0002$,
143 the first two symmetrical lasing wavelengths arise
144 when $\alpha = -2 \times 10^{-7}$, which correspond to the
145 amplification value ≈ 7 dB/m.

146 Along with investigations of reflectivity the de-
147 tailed analysis of reflective function phase spec-
148 trum has been carried out. Calculations show that

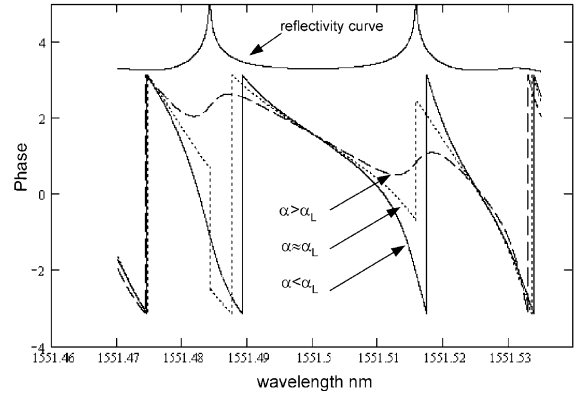


Fig. 5. Behavior of phase spectrum around lasing point.

149 the phase slope $\partial\phi/\partial\lambda$ is everywhere negative if the
150 gain is small, then it becomes steeper when the
151 gain increases, tending to the lasing value of gain
152 α_L , and becomes positive around the first lasing
153 wavelengths if gain exceeds the value needed for
154 lasing (Fig. 5). Then new regions with positive
155 phase slope are originating when pumping con-
156 tinue to increase as it is clearly seen in Fig. 6. Note
157 that conventional gratings always manifest the
158 negative phase slope independently of the sign of
159 chirp. Positive phase slope (or negative phase slope
160 with respect to frequency) is a rather unusual

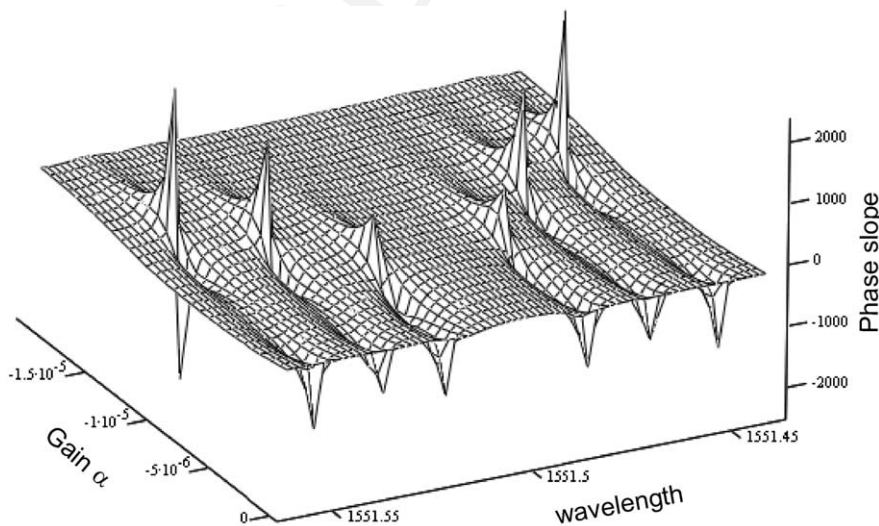


Fig. 6. Phase slope evolution versus gain and wavelength, $L = 5$ cm, $\mu = 0.000005$.

161 property, leading to some unique phenomenon,
162 which has recently drawn much interest. For ex-
163 ample, in a medium with positive phase slope a
164 superluminal propagation of a pulse amplitude has
165 been experimentally observed [9,10]. Positive
166 phase slope is the crucial item as well in the novel
167 method proposed to increase the performance of
168 interferometric sensors used for detecting ex-
169 tremely small displacements and rotation rates
170 [11,12].

171 4. Conclusions

172 Rare-earth-doped uniform FBG becomes a la-
173 ser when pumped with a definite pump rate. The
174 stronger is the FBG, the lower is the required
175 pump rate. By choosing an appropriate value of
176 pump rate, one can obtain a desirable lasing
177 wavelength within the set of their discrete values.
178 Such a laser can be used in a DWDM technique as
179 a booster with controlled lasing wavelengths, and
180 as a dual wavelength source for frequency shift
181 keying (FSK). Phase slope of the reflection func-
182 tion at small pumping is negative. By increasing
183 the pump, phase slope increases and then converts
184 to positive value. Such positive phase slope can be
185 used in novel experiments of superluminal propa-
186 gation of pulse amplitude as well as in the novel
187 method increasing the performance of interfero-
188 metric sensors. Over the last years several methods
189 have been studied to provide multi-wavelength
190 sources for WDM applications. Much effort has
191 been focused on dual and multiple wavelength
192 operation with the self-seeding approach, based on
193 wavelength selection in FBGs [13]. In this regard,
194 the proposed dual wavelength fiber laser can play
195 an important role as the number of channels in-
196 creases. FSK modulation versus traditional am-
197 plitude shift keying (ASK) can achieve smaller
198 channel spacing [14] and consequently higher
199 channel number in DWDM systems. FSK pre-
200 vents laser chirp, which have a destructive effect on
201 dispersion in long haul networks [15,16], and
202 proposed dual wavelength laser source can be a
203 good choice for those purposes.

Acknowledgements

204

This work was supported by the grant INTAS 205
97-30748. The results have discussed in seminar of 206
Photonics Research Group in Aston University, 207
Birmingham. Authors acknowledge Professor I. 208
Bennion and other participants for helpful dis- 209
cussions. 210

References

211

- [1] A. Othonos, K. Kalli, Fiber Bragg Gratings, Artech 212
House, Boston, London, 1999. 213
- [2] L. Dong, W.H. Loh, J.E. Caplen, J.D. Minelli, K. Shu, L. 214
Reekie, Opt. Lett. 22 (1977) 694. 215
- [3] W.H. Loh, B.N. Samson, L. Dong, G.J. Cowle, K. Hsu, J. 216
Lightwave Technol. 16 (1998) 114. 217
- [4] W.H. Louisell, Coupled Modes and Parametric Electron- 218
ics, John Wiley, New York, 1960. 219
- [5] L. Poladian, Phys. Rev. E-48 (1993) 4758. 220
- [6] G.G. Karapetyan, Microwave Opt. Technol. Lett. 20 221
(1999) 436. 222
- [7] H.V. Baghdasaryan, G.G. Karapetyan, T.M. Knyazyan, 223
S.T. Avagyan, N.K. Uzunoglu, in: COST 240 Workshop, 224
SOA-Based Components for Optical Networks, Prague, 225
1997. 226
- [8] H.V. Baghdasaryan, D.M. Meghavoryan, N. Uzunoglu, in: 227
Book of Abstracts. International Conference on Transpa- 228
rent Optical Networks – ICTON 2000, We.A.3, Poland, 229
2000. 230
- [9] E.L. Bolda, J.C. Garrison, R.Y. Chiao, Phys. Rev. A 49 231
(1994) 2938. 232
- [10] L.J. Wang, A. Kuzmich, A. Dogariu, Nature 406 (2000) 233
277. 234
- [11] G.G. Karapetyan, in: Proceedings of the Conference on 235
“Sensors and their applications XI”, London, September 236
2001, p. 303. 237
- [12] G.G. Karapetyan, Techn. Phys. 46 (10) (2001). 238
- [13] A. Laurent, P. Chanclou, M. Thual, J. Lostec, M. 239
Gadonna, J. Opt.: Pure Appl. Opt. A 2 (2000) L6. 240
- [14] C.S. Li, F.F. Tong, K. Lie, D.G. Messerschmitt, J. 241
Lightwave Technol. 10 (8) (1999) 1148. 242
- [15] R.S. Vodhanel, A.F. Elrefaie, R.E. Waghner, M.Z. Iqbal, 243
J.L. Gimlett, S. Tsuji, J. Lightwave Technol. 7 (10) (1989) 244
1454. 245
- [16] D. Marcuse, J. Lightwave Technol. 8 (7) (1990) 1110. 246